

Multi-technique combination for Earth Orientation & Reference Frames Determination

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and

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Combination at the Observation Level

Why combining at the Observation Level

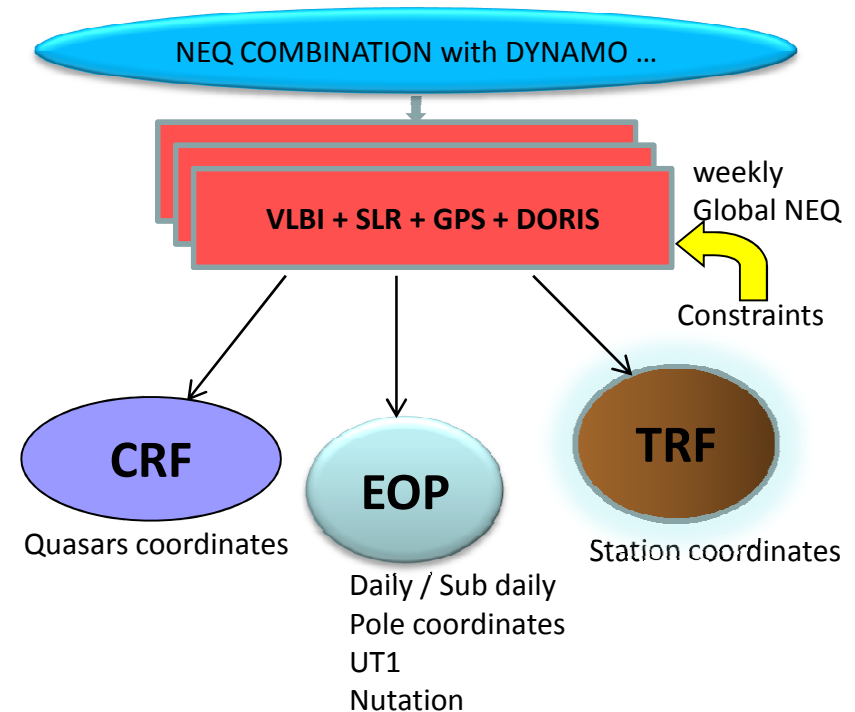
- Space geodetic techniques have different strengths and weaknesses for recovering geodetic parameters
- Some systematic behaviour which can easier and more efficiently be detected and reduced at the observation level.

Goal

- This could contribute to the IERS scope for a rigorous combination of ITRF, EOP and ICRF and ZTD.

How

- At the same epoch the observation equations from 4 space geodetic techniques GNSS, VLBI, SLR and DORIS are weekly stacked.
- Combination processes can be performed to determine common geodetic parameters



Combination at the Observation level or at the Normal Equation level

Actual equivalence between observation level and NEq level:

➔ Only technique independent parameters can be reduced

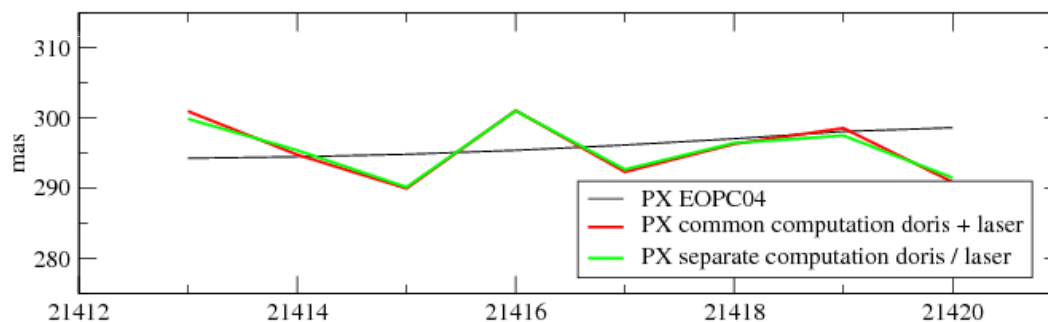
Test: Jason2 - 7 day arc

over the period

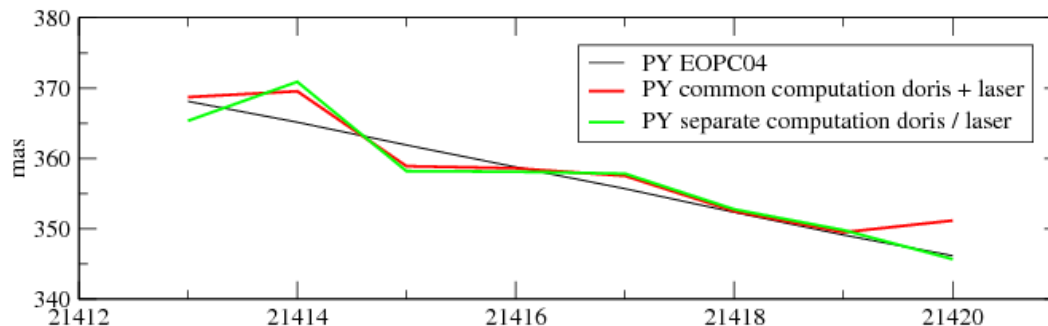
17/8/2008 – 23/8/2008

Technique	Nb of obs / eliminated obs	Residuals	Orbit # rms
SLR NEq	2216 / 224	4.1cm	12.1cm
DORIS NEq	109884 / 52825	.346mm/s	10.6cm
SLR + DORIS NEq	2247 / 193 109614 / 53095	4.2cm .352mm/s	

X-Pole



Y-Pole



Unconstrained Normal Equation

$$\underbrace{A^T \Pi A}_{N} \cdot \Delta p = \underbrace{A^T \Pi \Delta Q}_S \rightarrow N \cdot \Delta p = S$$

$$\Pi = \begin{pmatrix} \frac{1}{\sigma_1^2} & 0 & \cdot & \cdot & 0 \\ 0 & \frac{1}{\sigma_2^2} & \cdot & \cdot & 0 \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ 0 & \cdot & \cdot & \frac{1}{\sigma_{n-1}^2} & 0 \\ 0 & 0 & \cdot & 0 & \frac{1}{\sigma_n^2} \end{pmatrix}$$

weight Matrix with σ_i^2 uncertainty of observation i

NEq Reduction	NEq Weighted & Cumulated
$\begin{pmatrix} N_{II} & N_{IE}^T \\ N_{IE} & N_{EE} \end{pmatrix} \begin{pmatrix} \Delta p_I \\ \Delta p_E \end{pmatrix} = \begin{pmatrix} S_I \\ S_E \end{pmatrix}$ $\begin{cases} N_{II} \Delta p_I + N_{IE}^T \Delta p_E = S_I \\ N_{IE} \Delta p_I + N_{EE} \Delta p_E = S_E \end{cases}$ $\Delta p_I = N_{II}^{-1} (S_I - N_{IE}^T \Delta p_E)$ $N_{IE} N_{II}^{-1} (S_I - N_{IE}^T \Delta p_E) + N_{EE} \Delta p_E = S_E$ $\underbrace{(N_{EE} - N_{IE} N_{II}^{-1} N_{IE}^T)}_{N^\otimes} \Delta p_E = \underbrace{(S_E - N_{IE} N_{II}^{-1} S_I)}_{S^\otimes}$ $N^\otimes \cdot \Delta p_E = S^\otimes \text{ the reduced matrix}$	<p>for the i^{th} NEq: $N_i = A_i^T \Pi_i A_i$ and RHS term $S_i = A_i^T \Pi_i \Delta Q_i$ $N_i \cdot \Delta p = S_i$ π_i the weighting associated to N_i</p> $\underbrace{\left(\sum_{i=1}^k \pi_i N_i \right)}_N \Delta p = \underbrace{\left(\sum_{i=1}^k \pi_i S_i \right)}_S$ $N \cdot \Delta p = S$ $\pi_i = \frac{n_i}{\Delta Q_i^T \Pi_i \Delta Q_i}, \text{ with } n_i = \text{nb obs. of } i \text{ set}$ $\Pi_i = \text{diagonal matrix } 1/\sigma_j^2 \text{ for } j=1..n_i$ <p>or</p> $\pi_i = \text{calculated by iterative Helmert algorithm}$

Constrained Normal Equation

Continuity constraints on EOP

$$\Delta eop(t) - \Delta eop(t - \Delta t) = 0 \pm \sigma_{\text{constraint}}$$

Stability constraints on station coordinates (X_S, Y_S, Z_S)

$$\alpha_S \Delta X_S + \beta_S \Delta Y_S + \gamma_S \Delta Z_S = 0 \pm \sigma_S$$

Minimal constraints on transformation parameters

Translation	{	$T_X = 0 + \sigma_{\text{min}}, T_Y = 0 + \sigma_{\text{min}}, T_Z = 0 + \sigma_{\text{min}}$
Scale		$D = 0 + \sigma_{\text{min}}$
Rotation		$R_X = 0 + \sigma_{\text{min}}, R_Y = 0 + \sigma_{\text{min}}, R_Z = 0 + \sigma_{\text{min}}$

These constraints are pseudo observations converted in normal equation

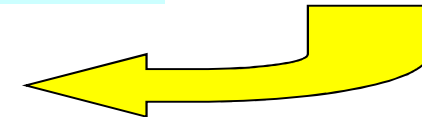
Local ties constraints on stations coordinates i and j

$$\begin{cases} \Delta X_{Si} - \Delta X_{Sj} = \Delta X_{Si-Sj} + \sigma_{Si-Sj} \\ \Delta Y_{Si} - \Delta Y_{Sj} = \Delta Y_{Si-Sj} + \sigma_{Si-Sj} \\ \Delta Z_{Si} - \Delta Z_{Sj} = \Delta Z_{Si-Sj} + \sigma_{Si-Sj} \end{cases}$$

$$N_c \cdot \Delta p = S_c$$

and added to the normal equation of observations

$$(N + N_c) \cdot \Delta p = S + S_c$$



Normal Equation Resolution

Determination of geodetic parameters using the Normal Equation Level

$$(\Delta \hat{p}) = N^{-1} S$$

Inverse Methods:

Explicit resolution

- Choleski
- Conjugate Gradients
- Singular Value Decomposition
- QR decomposition

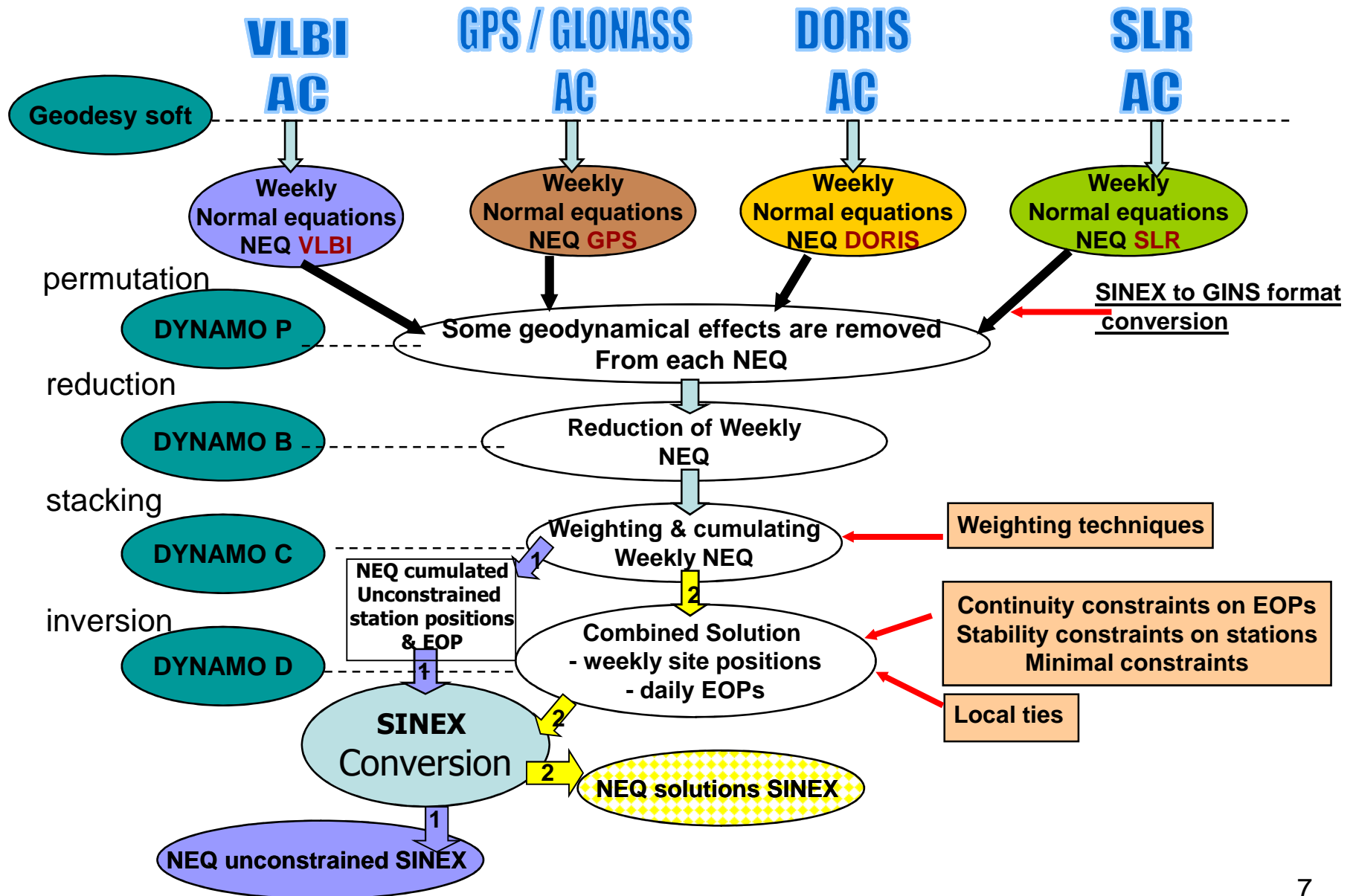
Householder orthogonal transformations

Givens rotation matrix

Iterative resolution

- Jacobi iteration
- Gauss-Seidel iteration
- Relaxation method

GRGS NEq Combination processing



Working Group on Combination at the Observation Level (COL)

Created in the frame of the IERS in October 2009

WG-COL Objectives

- Study methods and advantages of combining techniques (DORIS, GPS, SLR, VLBI) at the observation level
- Improve resolution and consistency of products (EOP, TRF, CRF) to increase accuracy of parameter determination
- Study technique dependent systematic errors
- Progress in combination methods and strategies (eg. weighting)
- Creating common standards for a rigorous combination
- Mutualize physical parameters (eg. troposphere)
- Extend the combination approach at the level of observation to several research groups in a planned IERS action
- Validate the rigorous combination approach vs. present realizations (C04, ITRF...)
- Prepare future of IERS

Working Group on Combination at the Observation Level (COL)

Project

- Compare the EOP solutions per technique & combined multi-techniques
- Compare the Stations Coordinates solutions
- Compare heterogeneous Software by inter-comparing results in parameters estimations

Benchmark

- August 10 to August 30, 2008 including the CONT08 VLBI period (12-26/08/08)
- based on weekly combined SINEX files from all space geodetic techniques together containing normal equations
- parameters

Geodetic Station coordinates

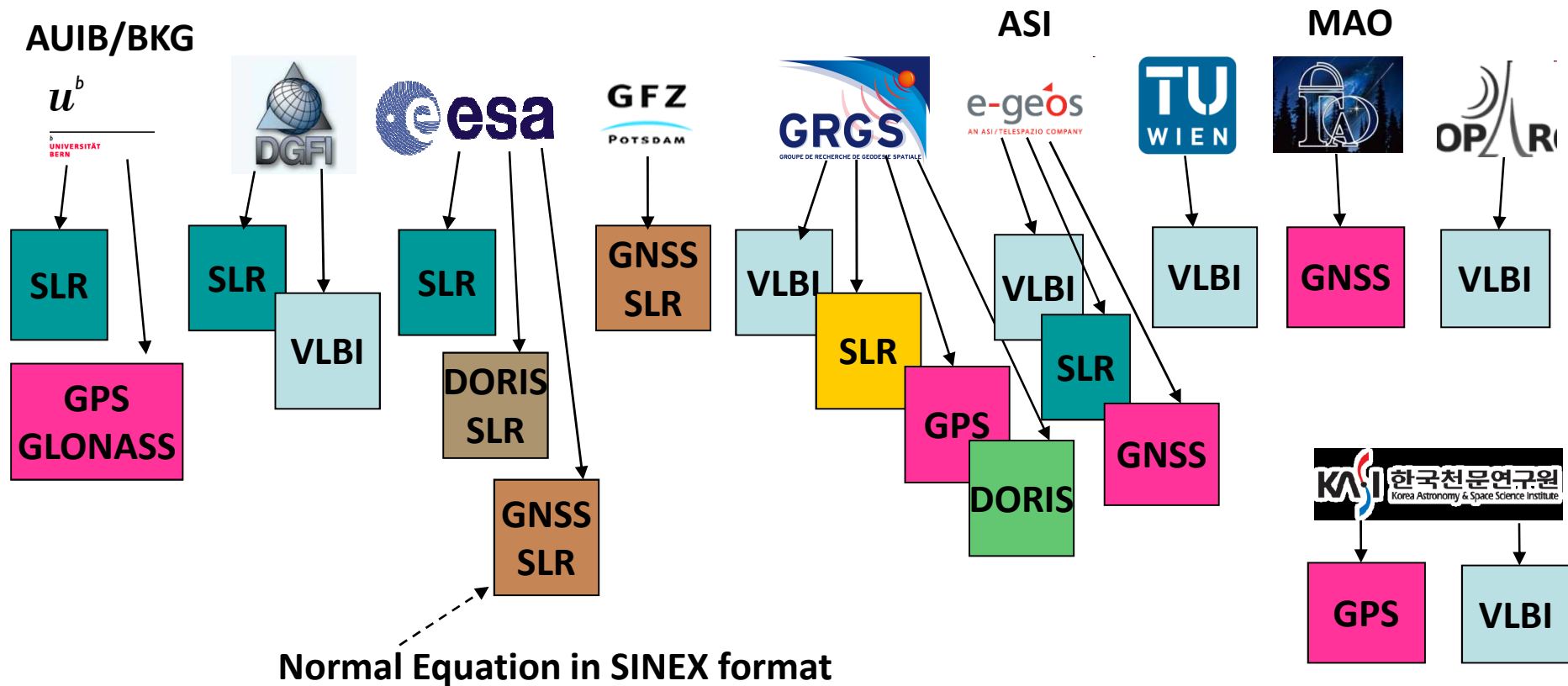
Polar motion

Nutation parameters

UT1

eventually Quasar coordinates and troposphere parameters

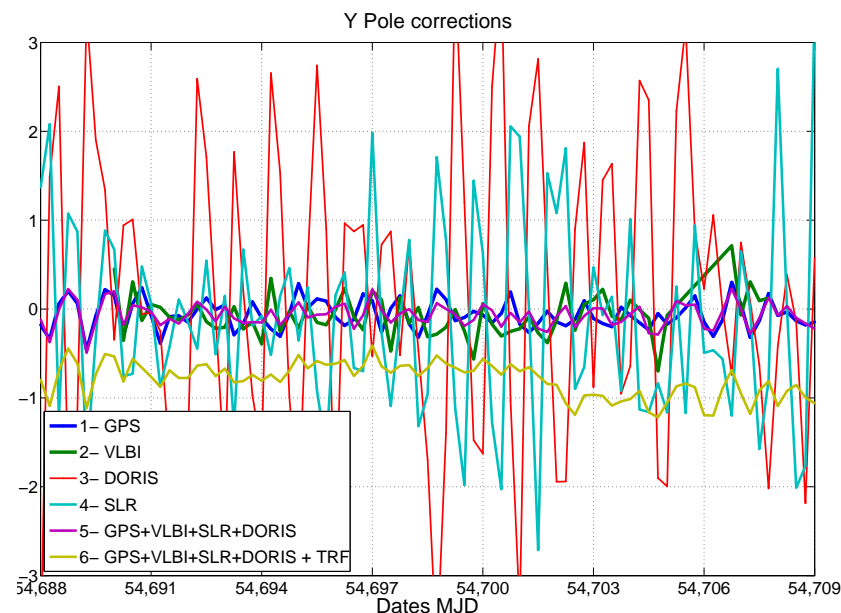
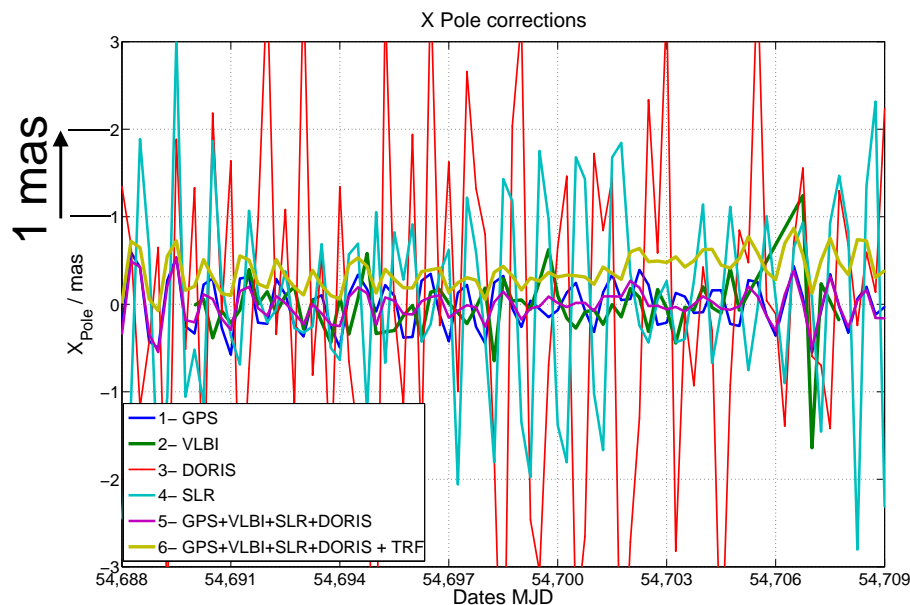
Centers participating to the COL comparison campaign and techniques performed per center



COL participants & softwares

Analysis Centers	Software
AIUB	BERNESE software as used by IGS AC CODE for GNSS
BKG	GEODYN software for SLR BERNESE + GIPSY software for GNSS CALC / SOLVE for VLBI
DGFI	DOGS 5.0 software for SLR, OCCAM 6.1 LSM + DOGS 5.0 for VLBI
ESOC	NAPEOS software
GFZ	EPOSOC 06.61 software
GRGS	GINS / DYNAMO software
ASI	GEODYN software
TUW	VieVS software for VLBI
MAO	CoCos Construct Combined Solution Software
JPL (potentially)	GIPSY / OASIS
GSFC (potentially)	GEODYN / SOLVE
Korea Astro Space Science Institute	

X and Y pole corrections from GRGS NEqs versus C04 series at 6h intervals over 3 weeks

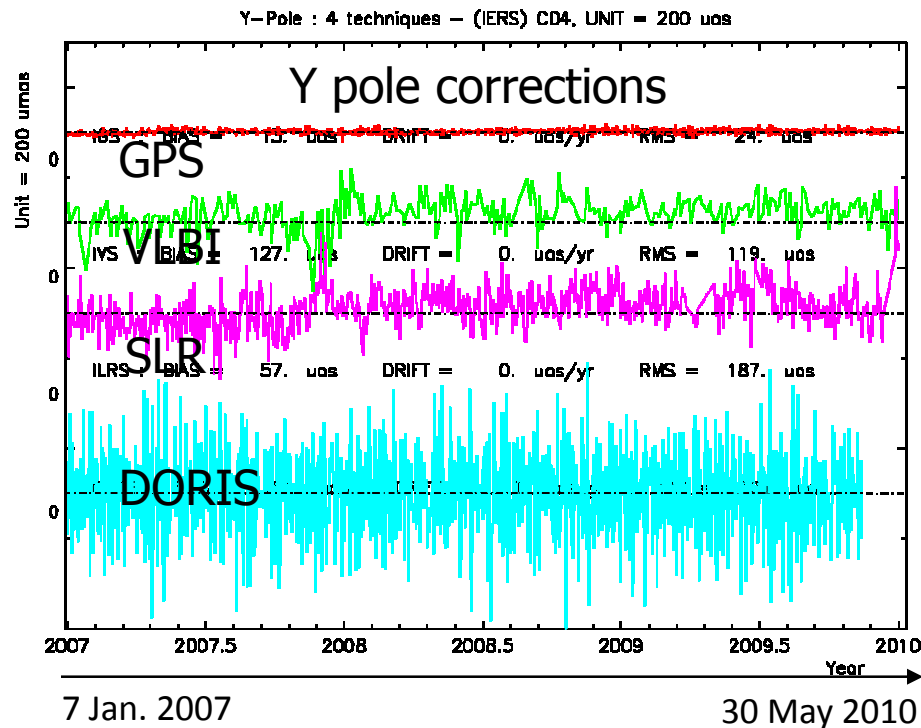


	Technique	Weighted Mean	Weighted RMS
X_Pole / μas	1- GPS	-10.3	160.6
	2- VLBI	-17.2	188.9
	3- DORIS	31.5	1484.7
	4- SLR	-25.7	855.2
	5- Combined	-10.0	165.6
	6- Combined +TRF	379.8	185.0

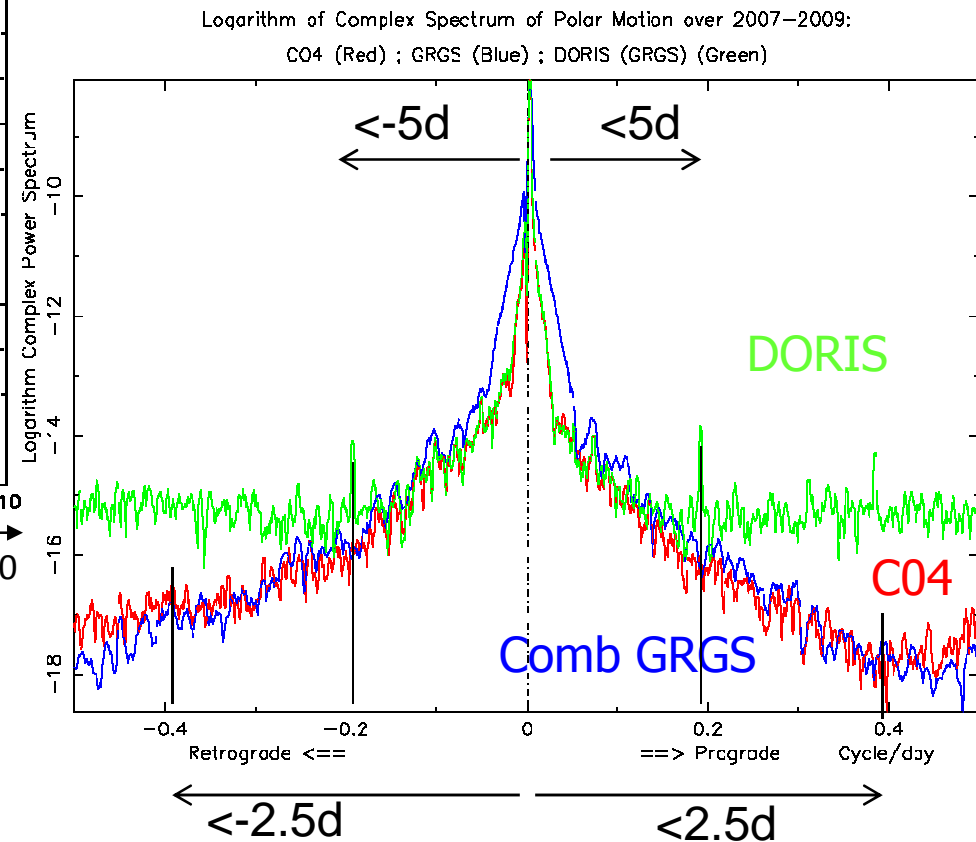
	Technique	Weighted Mean	Weighted RMS
Y_Pole / μas	1- GPS	-60.3	116.8
	2- VLBI	-91.7	174.2
	3- DORIS	262	1098.2
	4- SLR	-193	799.7
	5- Combined	-66.8	106.2
	6- Combined +TRF	-794	211.48

Daily Pole coordinates from DORIS technique versus C04 series at 1d intervals

X & Y pole series 1050 days -7 January 2007 to 30 May 2010



	DORIS
X pole mean	96 μas
Y pole mean	74 μas
X pole WRMS	650 μas
Y pole WRMS	519 μas



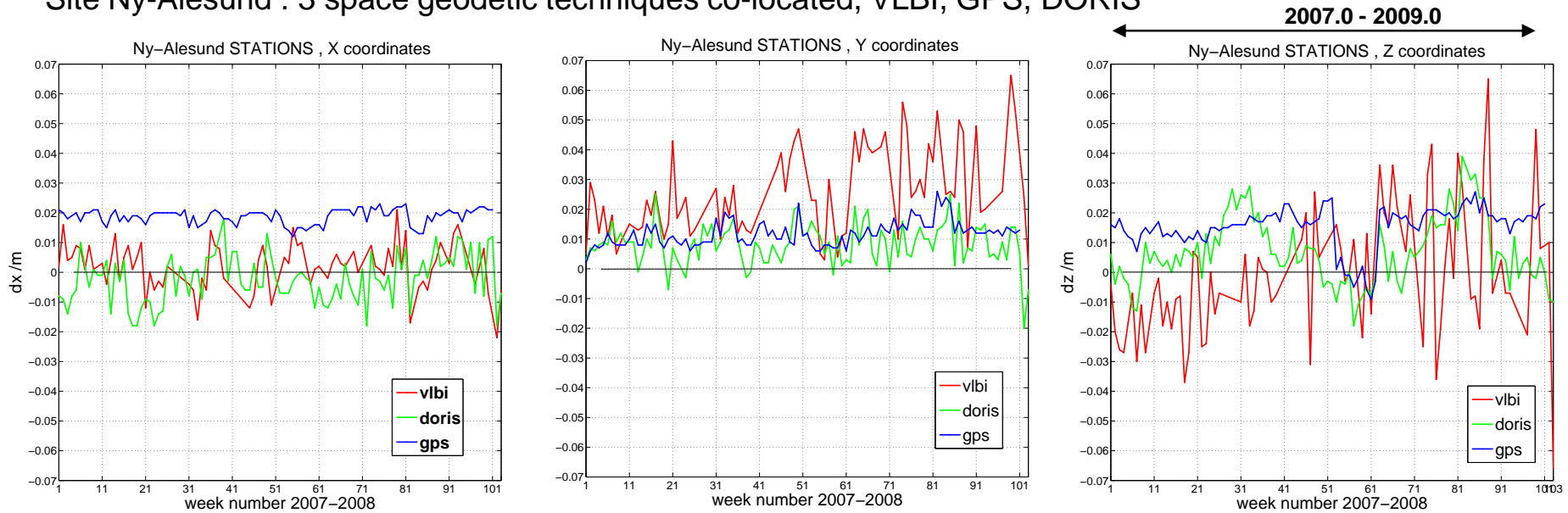
Station Coordinates

VLBI DORIS GPS Combination

Solutions by inversion of weekly unconstrained combined GPS SLR DORIS VLBI NEQ
 Pole UT & Nutation are fixed to the a priori **EOP C04 series**
 Weekly Terrestrial Station Coordinates are obtained with
 Systematic Constraints : $\sigma(S_x, S_y, S_z) = 1\text{m}$
 Minimal Constraints
 Ties Constraints on 26 co-located sites

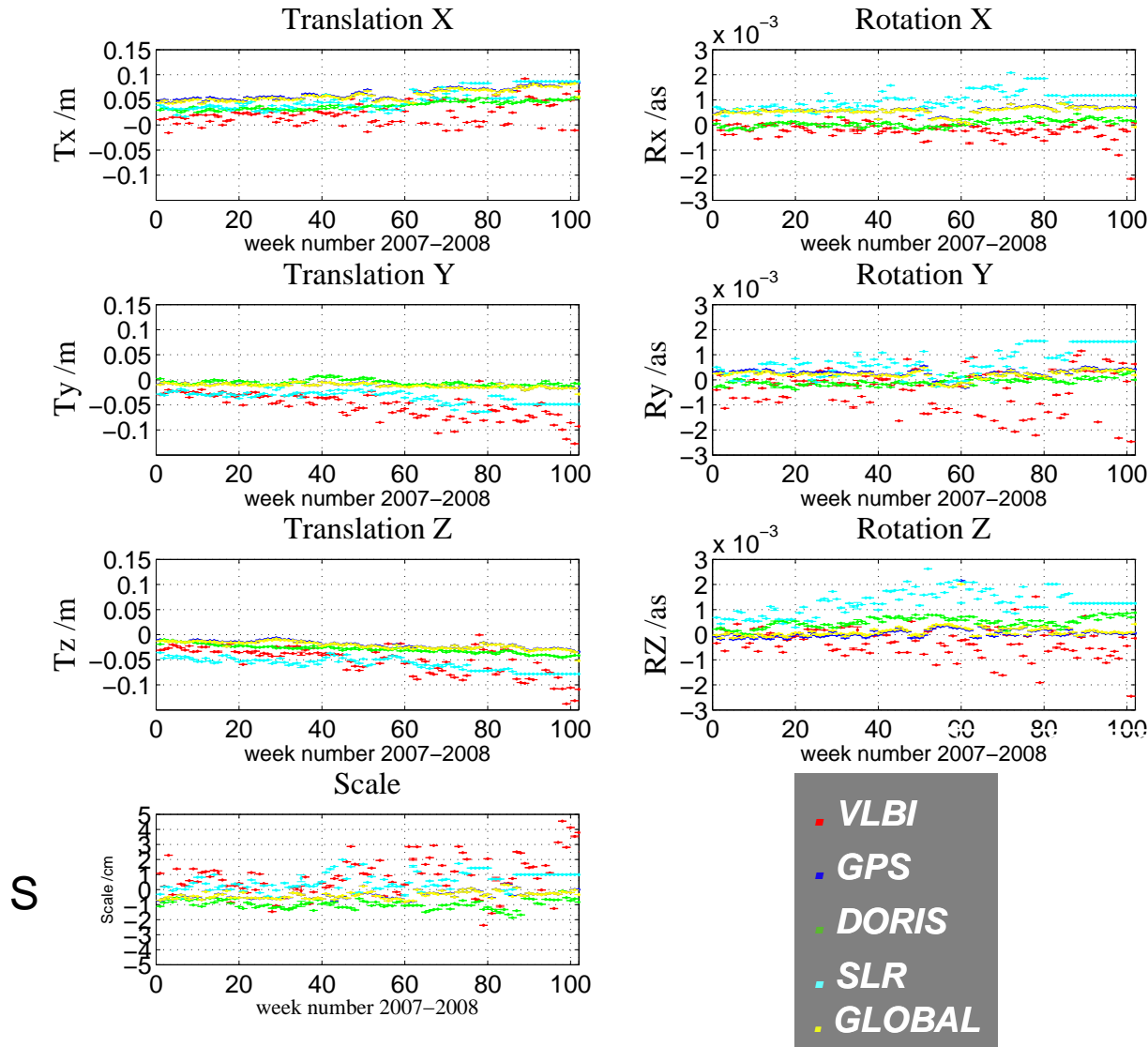


Site Ny-Alesund : 3 space geodetic techniques co-located, VLBI, GPS, DORIS



	\bar{X} / mm	\bar{Y} / mm	\bar{Z} / mm	$\langle (x - \bar{x})^2 \rangle / \text{mm}$	$\langle (y - \bar{y})^2 \rangle / \text{mm}$	$\langle (z - \bar{z})^2 \rangle / \text{mm}$	$d\bar{X} / \text{mm/y}$	$d\bar{Y} / \text{mm/y}$	$d\bar{Z} / \text{mm/y}$
VLBI	+ 2.0	+25.3	- 1.1	7.9	14.7	22.2	- 2.3	+19.5	+52.5
GPS	+18.8	+11.8	+15.4	2.5	4.2	6.9	- 4.0	+ 5.1	- 4.9
DORIS	- 2.2	+ 8.2	+ 6.9	8.1	7.0	11.4	+ 1.5	+ 6.7	+13.2

Transformation Parameters for GPS DORIS VLBI SLR and for GLOBAL combination with respect to ITRF2008



Transformation Parameters

Mean	DORIS Mean / σ	COMB Mean / σ
Tx cm	+3.9 / 0.8	+5.9 / 1.1
Ty cm	-0.6 / 0.5	-1.1 / 0.4
Tz cm	-2.9 / 0.8	-2.1 / 0.7
D cm	-0.99 / 0.29	-0.38 / 0.24
Rx μ as	+58.8 / 144	545 / 176
Ry μ as	-75.3 / 153	199 / 171
Rz μ as	+507 / 208	119 / 237

Rate	DORIS Rate / σ	COMB Rate / σ
Tx cm/y	+1.3 / 0.1	+1.7 / 0.2
Ty cm/y	-0.4 / 0.1	-0.5 / 0.1
Tz cm/y	-1.3 / 0.8	-1.1 / 0.1
D cm/y	-0.05 / 0.10	0.20 / 0.07
Rx μ as/y	156 / 39	62 / 59
Ry μ as/y	169 / 40	17 / 59
Rz μ as/y	213 / 58	126 / 78

COL-WG Prospect

- **Re-iterate the CONT08 campaign** with homogenized standards and parameters, a priori reference system ITRF2008, ICRF2, EOP-C04, IERS conventions 2010
- **NEq multi-techniques combination** weekly bases on CONT08 campaign for several participating ACs have to be compared
multi-technique combination from different ACs have to be performed
- **New sets of data:** LEO satellites
Jason-2 (SLR,DORIS,GPS multi-techniques on board)
GRACE (SLR,GPS two techniques on board)
- **Study the sub-diurnal EOP** variations by deriving hourly or 2-hours estimates
- **Interpolation method** of a-priori EOPC04 for the data epoch has to be adopted
- The next **participation meetings**
 - 25th general assembly of the IUGG (28 June - 07 July 2011)
 - 3rd international colloquium “Scientific and Fundamental Aspects of the Galileo Program” (31 August 02 September 2011)
 - “Journées de référence spatio-temporels” Paris September 2011
 - 3rd COL-WG meeting will be held at Paris (October 2011)
- **GRASP** space mission: “**G**eodetic **R**eference **A**ntenna in **S**pace” NASA’s Jet Propulsion Laboratory project will carry precise sensors system for GNSS, SLR, DORIS and VLBI geodetic techniques on space board satellite. The launch is expected in 2017.
- **HY-2A** satellite mission using the SLR GPS and DORIS technique on board

Thanks for your attention